

# Modes of Vibration of Volcano tube. W/S McVitt

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MRN 016

acoustic equation  $\omega^2 p + \alpha^2 \nabla^2 p + \lambda \nabla p \cdot \nabla \frac{1}{\rho} = 0$

in one dimension  $\alpha^2 \frac{d^2 p}{dz^2} + \lambda \frac{d \frac{1}{\rho}}{dz} \frac{dp}{dz} + \omega^2 p = 0$

$$\alpha^2 = \frac{\lambda}{\rho} \quad \frac{d}{dz} \rho^{-1} = -\rho^{-2} \frac{d\rho}{dz}$$

$$\frac{\lambda}{\rho} \frac{d^2 p}{dz^2} - \frac{\lambda}{\rho^2} \frac{d\rho}{dz} \frac{dp}{dz} + \omega^2 p = 0$$

$$\lambda \rho \frac{d^2 p}{dz^2} - \lambda \frac{d\rho}{dz} \frac{dp}{dz} + \omega^2 \rho^2 p = 0$$

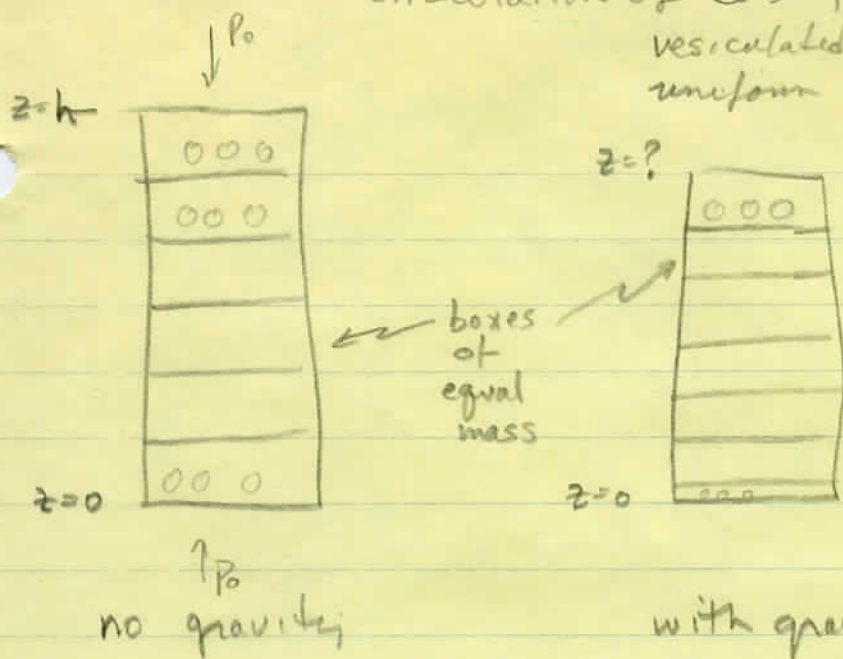
$$\frac{d^2 p}{dz^2} - \frac{1}{\rho} \frac{d\rho}{dz} \frac{dp}{dz} + \omega^2 \frac{\rho}{\lambda} p = 0$$

$$\frac{d^2 p}{dz^2} + f_1(z) \frac{dp}{dz} + \omega^2 f_2(z) p = 0$$

$$f_1(z) = -\frac{1}{\rho} \frac{d\rho}{dz} \quad \int \frac{d\rho}{\rho} = \int f_1(z) dz = \ln(\rho)$$

$$f_2(z) = \frac{\rho}{\lambda} \quad \rho = \rho_0 e^{\int_0^z f_1(z') dz'} \quad \lambda = \frac{\rho}{f_2(z)}$$

calculation of density profile in vesiculated lava tube having a uniform concentration of gas (ideal)



let boxes have unknown height  $dz$  and known mass  $dm$   
 ideal gas law for vesicles  $PV = \text{constant}$   
 let boxes have volume  $dV = dV_g + dV_f$

volume of vesicles at pressure  $P$   $dV_g = \frac{P_0 dV_g^0}{P}$

volume of incompressible fluid at pressure  $P$   $dV_f = dV_f^0$

initial volumes  $V^0$  given by porosity  $dV = \left( (1-n_0) + \frac{n_0 P_0}{P} \right) dV^0$

height of box  $dz$  is just its volume (given unit area tube)

$$dz = \left\{ (1-n_0) + \frac{n_0 P_0}{P} \right\} dV^0$$

initial volume related to initial bulk density and mass  $dV^0 = \frac{dm}{\rho_b^0}$

$$dz = \left\{ (1-n_0) + \frac{n_0 P_0}{P} \right\} \frac{dm}{\rho_b^0}$$

pressure at any point weight of overlying material  $P = P_0 + \rho_b^0 g h - g m$

where  $m = \int_0^m dm \equiv$  mass of material below box

$$dz = \frac{1}{\rho_b^0} \left\{ (1-n_0) + \frac{n_0 P_0}{P_0 + \rho_b^0 g h - g m} \right\} dm$$

$$\int_0^z dz \approx z = \int_0^m \frac{1}{\rho_b^0} \left\{ (1-n_0) + \frac{n_0 P_0}{P_0 + \rho_b^0 g h - g m} \right\} dm$$

This gives

$$z = \frac{(1-n_0)}{\rho_b^0} m - \frac{n_0 P_0}{\rho_b^0 g} \log \left\{ (P_0 + \rho_b^0 g h) - g m \right\} + \frac{n_0 P_0}{\rho_b^0 g} \log(P_0 + \rho_b^0 g h)$$

int. const.

new bulk density =  $\left( \frac{dm}{dz} \right)$

$$\rho_{\text{bulk}}(z) = \frac{dm}{dz} = \rho_b^0 \left\{ (1-n_0) + \frac{n_0 P_0}{(P_0 + \rho_b^0 g h) - g m(z)} \right\}^{-1}$$

where  $m(z)$  is such that

$$z(m) = \frac{(1-n_0)}{\rho_b^0} m + \frac{n_0 P_0}{\rho_b^0 g} \log \left\{ \frac{(P_0 + \rho_b^0 g h) - g m}{(P_0 + \rho_b^0 g h)} \right\}$$

$$z = \text{top} \quad m = \rho_b^0 h$$

$$z_{\text{top}} = (1-n_0)h - \frac{n_0 P_0}{\rho_b^0 g} \left\{ \log(P_0) - \log(P_0 + \rho_b^0 g h) \right\}$$

$$z_{\text{top}} = (1-n_0)h + \frac{n_0 P_0}{\rho_b^0 g} \log \left\{ 1 + \frac{\rho_b^0 g h}{P_0} \right\}$$

$$\lim_{g \rightarrow 0} z = h$$

$$\lim_{n_0 \rightarrow 0} z = h$$



porosity

gas	$n$	$\rho_g$	$\lambda_g$
fluid	$(1-n)$	$\rho_f$	$\lambda_f$

$$\frac{\text{mass}}{\text{volume}} = \frac{n\rho_g + (1-n)\rho_f}{1}$$

$$\rho_{\text{bulk}} = n\rho_g + (1-n)\rho_f$$

$$= \rho_f - (\rho_f - \rho_g)n$$

$$= \rho_f - \Delta\rho n$$

$$p = -\lambda \nabla \cdot u$$

$$\nabla \cdot u = \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = \text{volumetric strain}$$

$$\text{volumetric strain} = \frac{\text{new volume} - \text{orig volume}}{\text{orig volume}}$$

gas	$n$	$\lambda_g$
fluid	$(1-n)$	$\lambda_f$

$$\text{orig volume} = 1$$

suppose pressure is  $p$ . Then since pressure uniform then volume strain in gas is  $\nabla \cdot u = -p\lambda_g^{-1}$  and strain in fluid is  $\nabla \cdot u = -p\lambda_f^{-1}$ . so

$$-p\lambda_g^{-1} = -\frac{n + V_{\text{new}}^g}{n}$$

$$-p\lambda_f^{-1} = -\frac{(1-n) + V_{\text{new}}^f}{(1-n)}$$

$$V_{\text{new}}^g = -n p \lambda_g^{-1} + n$$

$$V_{\text{new}}^f = -(1-n)p\lambda_f^{-1} + (1-n)$$

$$\text{total new volume} = -n p \lambda_g^{-1} - (1-n)p\lambda_f^{-1} + 1$$

$$\text{bulk strain} = -p \left[ \frac{n}{\lambda_g} + \frac{(1-n)}{\lambda_f} \right]$$

$$\lambda_{\text{bulk}} = \left[ \frac{n}{\lambda_g} + \frac{(1-n)}{\lambda_f} \right]^{-1}$$

$$\rho_{\text{bulk}} = \rho_f - [\rho_f - \rho_g]n$$

$$\lambda_{\text{bulk}} = \left[ \frac{1}{\lambda_f} + \left( \frac{1}{\lambda_g} - \frac{1}{\lambda_f} \right) n \right]^{-1}$$

suppose  $p_{\text{bulk}} = a + bn$

$$\lambda_{\text{bulk}}^{-1} = c + dn$$

$$f_1 = -b(a + bn)^{-1} \frac{dn}{dz}$$

$$f_2 = (a + bn)(c + dn) = ac + (ad + bc)n + bd n^2$$

\* note: Hillebrand, Meth of App Math P 145

given  $\frac{d}{dx} (P \frac{dy}{dx}) + qy + \lambda ry = 0$

y prescribed at ends  
or y' = 0 at ends

Then  $\lambda = \frac{\int_a^b (py'^2 - qy^2) dx}{\int_a^b ry^2 dx}$

and  $\lambda$  stationary w.r.t.  
variations in y.

in acoustics

$\nabla \cdot u = -\frac{p}{\lambda}$

$\ddot{u} = -\frac{1}{\rho} \nabla p$

$\nabla \cdot (\frac{1}{\rho} \nabla p) + \frac{\omega^2}{\lambda} p = 0$

$\frac{d}{dz} (\frac{1}{\rho} \frac{dp}{dz}) + \frac{1}{\lambda} \omega^2 p = 0$

$\omega^2 = \frac{\int \frac{1}{\rho} (\frac{dp}{dz})^2 dz}{\int \frac{1}{\lambda} p^2 dz} = \frac{I_1}{I_2}$

$$\omega^2 = I_1 I_2^{-1} \quad \text{let } p = \sum c_i \phi_i$$

$$\frac{\partial \omega^2}{\partial c_i} = 0 = \frac{\frac{\partial I_1}{\partial c_i} I_2 - I_1 \frac{\partial I_2}{\partial c_i}}{I_2^2}$$

assume  $I_2 \neq 0$

$$0 = \frac{\partial I_1}{\partial c_i} I_2 - I_1 \frac{\partial I_2}{\partial c_i} \quad \text{divide by } I_2$$

$$0 = \frac{\partial I_1}{\partial c_i} - \omega^2 \frac{\partial I_2}{\partial c_i}$$

$$\text{let } I_{2ij} = \int \frac{1}{\lambda} \phi_i \phi_j dz \quad I_{1ij} = \int \frac{1}{\rho} \phi_i' \phi_j' dz$$

$$I_1 = \sum_j \sum_k c_j c_k I_{1jk} \quad I_2 = \sum_j \sum_k c_j c_k I_{2jk}$$

$$\frac{\partial I_1}{\partial c_i} = 2 \sum_k c_k I_{1ik}$$

$$\frac{\partial I_2}{\partial c_i} = 2 \sum_k c_k I_{2ik}$$

$$\begin{bmatrix} I_{111} & I_{112} & I_{113} & \dots \\ I_{121} & & & \end{bmatrix} \begin{bmatrix} c_1 \\ c_2 \\ c_3 \\ \vdots \end{bmatrix} = \omega^2 \begin{bmatrix} I_{211} & \dots \\ \vdots \\ \vdots \end{bmatrix} \begin{bmatrix} c_1 \\ c_2 \\ c_3 \\ \vdots \end{bmatrix}$$

$$\underline{I_1} \underline{c} = \omega^2 \underline{I_2} \underline{c}$$

$$\boxed{\underline{I_2}^{-1} \underline{I_1} \underline{c} = \omega^2 \underline{c}}$$





$$p = \sum_{n=1}^{\infty} c_n \cos \left[ (n - \frac{1}{2}) \pi z / h \right]$$

$$\phi_n = \cos \left[ \frac{(n - \frac{1}{2}) \pi}{h} z \right]$$

$$\phi'_n = - \frac{(n - \frac{1}{2}) \pi}{h} \sin \left[ \frac{(n - \frac{1}{2}) \pi}{h} z \right]$$

$$I_{2ij} = \int_0^h \frac{1}{\lambda} \cos \left[ \frac{(i - \frac{1}{2}) \pi z}{h} \right] \cos \left[ \frac{(j - \frac{1}{2}) \pi z}{h} \right] dz$$

$$I_{1ij} = \frac{(i - \frac{1}{2})(j - \frac{1}{2}) \pi^2}{h^2} \int_0^h \frac{1}{\rho} \sin \left[ \frac{(i - \frac{1}{2}) \pi z}{h} \right] \sin \left[ \frac{(j - \frac{1}{2}) \pi z}{h} \right] dz$$

note  $I_{11}$ ,  $I_{22}$  symmetric.



for homogeneous media

$$I_{2ii} = \frac{1}{\lambda} \int_0^h \cos^2 \left[ \frac{(i-1/2)\pi z}{h} \right] dz = \frac{1}{\lambda} \frac{h}{2}$$

$$I_{1ii} = \frac{\pi^2 (i-1/2)^2}{h^2} \frac{1}{\rho} \int_0^h \sin^2 \left[ \frac{(i-1/2)\pi z}{h} \right] dz = \frac{\pi^2 (i-1/2)^2}{h^2} \frac{1}{\rho} \frac{h}{2}$$

$$\underline{I}_1 \underline{C} = \omega^2 \underline{I}_2 \underline{C}$$

matrices diagonal, therefore:

$$\omega_i^2 = \frac{I_{1,ii}}{I_{2,ii}} = \frac{\lambda}{\rho} \frac{\pi^2 (i-1/2)^2}{h^2}$$

$$\omega_i = \sqrt{\frac{\lambda}{\rho}} \frac{\pi (i-1/2)}{h}$$

$$= \frac{\alpha \pi}{h} (i-1/2)$$

$$\alpha = \sqrt{\frac{\lambda}{\rho}}$$

$$\frac{\pi^2}{2} \left(\frac{1}{2}\right)^2 = 1.234$$

$$\frac{\pi^2}{2} \left(\frac{3}{2}\right)^2 = 11.109$$

$$\frac{\pi^2}{2} \left(\frac{5}{2}\right)^2 = 30.842$$

from physical reasoning

$$\alpha = \lambda_i f_i = \frac{\lambda_i \omega_i}{2\pi} \quad \lambda_i = \frac{2h}{(i-1/2)}$$

$$\omega_i = \frac{2\pi \alpha}{\lambda_i} = \frac{2\pi \alpha}{2} \frac{(i-1/2)}{h} = \frac{\alpha \pi}{h} (i-1/2)$$

which checks.

$$\omega_i = \frac{\alpha \pi}{h} (i-1/2)$$

$$f_i = \frac{\omega}{2\pi} = \frac{\alpha}{2h} (i-1/2)$$

$$\text{if } \alpha = h = 1$$

$$f_1 = \frac{1}{4}$$

$$f_2 = \frac{3}{2} \cdot \frac{1}{2} = \frac{3}{4}$$

$$f_3 = \frac{5}{2} \cdot \frac{1}{2} = \frac{5}{4}$$

set up problem in terms of perturbations.

$$\text{let } \frac{1}{f} = \frac{1}{f_0} + f_p(z)$$

$$\frac{1}{\lambda} = \frac{1}{\lambda_0} + f_\lambda(z)$$

$$I_{2ij} = \int_0^h \frac{1}{\lambda_0} \cos \left[ \frac{(i-1/2)\pi z}{h} \right] \cos \left[ \frac{(j-1/2)\pi z}{h} \right] dz + \int_0^h f_p(z) \cos \left[ \frac{(i-1/2)\pi z}{h} \right] \cos \left[ \frac{(j-1/2)\pi z}{h} \right] dz$$

$$= I_{2ij}^0 + I_{2ij}^1$$

$$I_{1ij} = I_{1ij}^0 + I_{2ij}^1 \quad ?$$

# Test Case VARIATIONAL procedure

\*

$$h = 1.0 \text{ km}$$

$$\frac{\times 10^{15} \text{ g}}{\text{km}^2 \text{ sec}} \quad \times \frac{10^{15} \text{ g}}{\text{km}^3}$$

$$\lambda, \rho \text{ gas} = 0.5, 0.5 \quad \text{ie} \quad \kappa_{\text{fluid}} = 1.0 \text{ km/sec}$$

$$\lambda, \rho \text{ fluid} = 18, 2 \quad \text{ie} \quad \lambda_{\text{gas}} = 3.0 \text{ km/sec}$$

100 integration pts

case 1

$$p = 0.5$$

constant case 2  $\lambda = 0.5$

$$p = 0.4 + 0.2z$$

case 3

$$p = 0.2 + 0.6z$$

0	0.22056 } .4414	0.23503 } .43457	0.27186 } .44281
1	0.66196	0.66960	0.71467
2	1.1028	1.1108	1.1680
3	1.5440	1.5530	1.6237
4	1.9851 } .4411	1.9955 } .4427	2.0801 } .4608
5	2.4262 } .4411	2.4382	2.5409
6	2.8673	2.8805	2.9961

# The 3<sup>d</sup> lava tube in all its glory

①

acoustic eqn  $\nabla \cdot \left( \frac{1}{\rho} \nabla p \right) + \frac{\omega^2}{\lambda} p = 0$

$$\nabla p = \frac{\partial p}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial p}{\partial \phi} \hat{\phi} + \frac{\partial p}{\partial z} \hat{z}$$

$$\rho = \rho(z) \\ \lambda = \lambda(z)$$

$$\nabla \cdot \underline{f} = \frac{1}{r} \frac{\partial}{\partial r} (r f_r) + \frac{1}{r} \frac{\partial f_\phi}{\partial \phi} + \frac{\partial f_z}{\partial z}$$

$$\frac{1}{\rho} \nabla p = \frac{1}{\rho} \frac{\partial p}{\partial r} \hat{r} + \frac{1}{\rho r} \frac{\partial p}{\partial \phi} \hat{\phi} + \frac{1}{\rho} \frac{\partial p}{\partial z} \hat{z}$$

$$\nabla \cdot \left( \frac{1}{\rho} \nabla p \right) = \frac{1}{\rho r} \frac{\partial}{\partial r} \left( r \frac{\partial p}{\partial r} \right) + \frac{1}{\rho r^2} \frac{\partial^2 p}{\partial \phi^2} + \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial p}{\partial z} \right)$$

so equation is

$$\frac{1}{\rho r} \frac{\partial}{\partial r} \left( r \frac{\partial p}{\partial r} \right) + \frac{1}{\rho r^2} \frac{\partial^2 p}{\partial \phi^2} + \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial p}{\partial z} \right) + \frac{\omega^2}{\lambda} p = 0$$

let  $p = R(r) \Phi(\phi) Z(z)$

$$0 = \frac{1}{\rho r} \Phi(\phi) Z(z) \frac{\partial}{\partial r} \left( r \frac{\partial R}{\partial r} \right) + \frac{1}{\rho r^2} R Z \frac{\partial^2 \Phi}{\partial \phi^2} + R \Phi \frac{d}{dz} \left( \frac{1}{\rho} \frac{dZ}{dz} \right) + \frac{\omega^2}{\lambda} R \Phi Z$$

divide through by  $p$  multiply by  $\rho$  rearrange terms

$$-\frac{1}{rR} \frac{d}{dr} \left( r \frac{dR}{dr} \right) - \frac{1}{r^2 \Phi} \frac{d^2 \Phi}{d\phi^2} = \frac{\rho}{Z} \frac{d}{dz} \left( \frac{1}{\rho} \frac{dZ}{dz} \right) + \frac{\rho \omega^2}{\lambda}$$

so these terms equal to a constant, say  $\gamma^2$





input

$h =$  length of pipe

$nh =$  number of sampling points from  
0 to  $h$

por = porosity, a function of  $h$

$$\frac{\rho}{r^2} \frac{1}{\lambda} \left( \frac{1}{\rho} \frac{d^2 Z}{dz^2} \right) + \frac{\rho \omega^2}{\lambda} - \gamma^2 = 0$$

$$\frac{1}{r R} \frac{d}{dr} \left( r \frac{\partial R}{\partial r} \right) + \frac{1}{r^2 \Phi} \frac{d^2 \Phi}{d\phi^2} + \gamma^2 = 0$$

multiply by  $r^2$  and rearrange

$$\frac{r}{R} \frac{d}{dr} \left( r \frac{\partial R}{\partial r} \right) + r^2 \gamma^2 = - \frac{1}{\Phi} \frac{d^2 \Phi}{d\phi^2}$$

so these equal to a constant say  $m^2$

$$\frac{r}{R} \frac{d}{dr} \left( r \frac{\partial R}{\partial r} \right) + r^2 \gamma^2 = m^2$$

$$\frac{d^2 \Phi}{d\phi^2} = -m^2 \Phi$$

this second equation can be solved to give  $\Phi = e^{\pm im\phi}$   
but since physically  $e^{\pm im\phi} = e^{\pm i\lambda(\phi + 2\pi)}$  we  
must have  $e^{\pm 2\pi m i} = 1$  or  $m = 0, 1, 2, \dots$

the  $r$  equation is then  $r \frac{dR}{dr} + r^2 \frac{d^2 R}{dr^2} + (r^2 \gamma^2 - m^2) R = 0$

$m:$   
$$r^2 \frac{d^2 R}{dr^2} + r \frac{dR}{dr} + (r^2 \gamma^2 - m^2) R = 0$$

comparing to the form Heibronnd gives:

$a=1$   $b=0$   $c=-m^2$   $d=r^2$   $s=1$  and the soln is

$R = J_m(\gamma r)$  but the boundary conditions at

the rigid surface of the cylinder so that the normal derivative of the pressure is zero. i.e.  $\nabla p \cdot \hat{r} = \frac{\partial p}{\partial r} = 0$  so that we must choose  $Y$  so that this condition holds at  $r=a$  = cylinder's surface. Suppose  $\pi_{me}$  give the value of  $\alpha$  of the  $l$ -th (maxima - minima) of the  $m$ -th Bessel function  $J_m(r)$ . Then  $\alpha a = \pi_{me}$  and

$$R = J_m\left(\frac{\pi_{me}}{a} r\right) \quad Y = \frac{\pi_{me}}{a}$$

note, since  $J_0(0)$  satisfies eqn  $\nabla p = 0$

getting back to the  $Z$  equation. we have

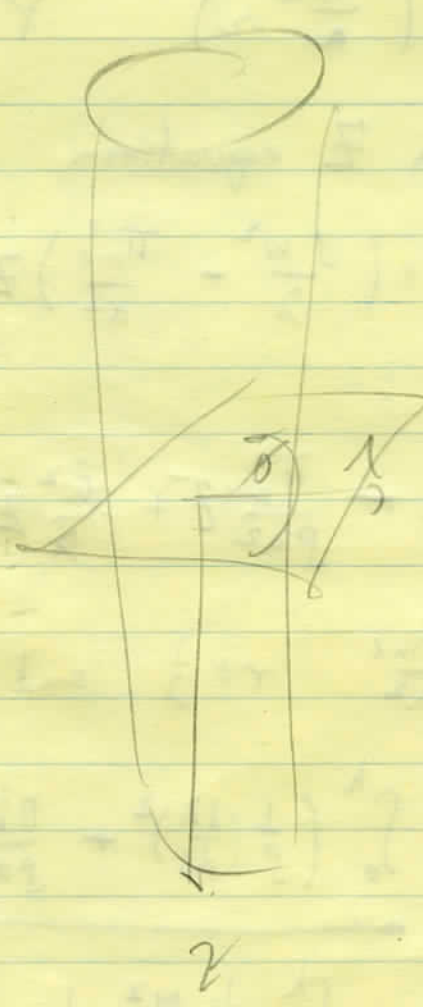
$$\rho \frac{d}{dz} \left( \frac{1}{\rho} \frac{dz}{dz} \right) + \left( \frac{\rho \omega^2}{\lambda} - \frac{\pi_{me}^2}{a^2} \right) Z = 0$$

or

$$\frac{d}{dz} \left( \frac{1}{\rho} \frac{dz}{dz} \right) - \frac{\pi_{me}^2}{\rho a^2} Z + \frac{\omega^2}{\lambda} Z = 0$$

note  $P = \frac{1}{\rho}$   $Q = -\frac{\pi_{me}^2}{\rho a^2}$   $r = \frac{1}{\lambda}$  and variational integral is

$$\omega^2 = \frac{\int_0^h \left( \frac{1}{\rho} \left( \frac{dz}{dz} \right)^2 + \frac{\pi_{me}^2}{\rho a^2} Z^2 \right) dz}{\int_0^h \frac{1}{\lambda} Z^2 dz}$$





(4)

now suppose  $\rho, \lambda$  constants, then

$$\frac{d^2 \zeta}{dz^2} + \left( \frac{\rho}{\lambda} \omega^2 - \frac{\pi^2 m^2}{a^2} \right) \zeta = 0$$

let  $\delta^2 = \frac{\rho}{\lambda} \omega^2 - \frac{\pi^2 m^2}{a^2}$  so that equation becomes

$$\frac{d^2 \zeta}{dz^2} + \delta^2 \zeta = 0$$

solution with boundary conditions rigid at  $z=0$ , pressure free at  $z=h$  is

$$\zeta = \cos(\delta z) = \cos\left(\frac{(n+1/2)\pi}{h} z\right) \quad n=0, 1, 2, \dots$$

$$\delta^2 = \frac{(n+1/2)^2 \pi^2}{h^2} = \frac{\rho}{\lambda} \omega^2 - \frac{\pi^2 m^2}{a^2}$$

or

$$\omega = \alpha \sqrt{\frac{(n+1/2)^2 \pi^2}{h^2} + \frac{\pi^2 m^2}{a^2}}$$

$$p_{mem} = \cos\left[\frac{(n+1/2)\pi z}{h}\right] J_m\left(\frac{\pi m r}{h}\right) e^{\pm im\theta}$$

$$\omega = \alpha \sqrt{\frac{(n+1/2)^2 \pi^2}{h^2} + \frac{\pi^2 m^2}{a^2}}$$

$$n, m, l = 0, 1, 2, \dots$$

in order of size

<u>me</u>	<u>Time</u>
0,0	0.0000
1,0	1.8413
2,0	3.0544
0,1	3.8316
3,0	4.2012
4,0	5.3172
1,1	5.3315
4,0	6.4122
2,1	6.7067
0,3	7.0015
5,0	7.4122
3,1	8.0178
2,0	8.4707
1,2	8.5363
4,1	9.2893
7,0	9.3325
2,2	9.9695

Table of Time  $\leq 10.0$

m/l	0	1	2	3
0	0	3.8316	7.0155	10.1735
1	1.8412	5.3315	8.5363	11.7060
2	3.0544	6.7067	9.9695	13.1704
3	4.2012	8.0148	11.3462	14.5859
4	5.3172	9.2893	12.6828	15.9643
5	6.4122	10.5339	13.9894	17.3136
6	7.4777	11.7593	15.2727	
7	8.4707	14.1705		
8	9.3325	15.3621		
9	10.0616			
10				

(6)

setting up the eigenvalue problem

$$\text{we have } 0 = \frac{\partial I_1}{\partial c_i} - \omega^2 \frac{\partial I_2}{\partial c_i}$$

$$I_1 = \int \frac{1}{\rho} \left( \frac{dz}{dz} \right)^2 dz + \frac{\pi^2 m e}{a^2} \int \frac{1}{\rho} z^2 dz = I_{1A} + \frac{\pi^2 m e}{a^2} I_{1B}$$

$$I_2 = \int \frac{1}{\lambda} z^2 dz$$

$$\text{let } I_{1Aij} = \int_0^h \frac{1}{\rho} \phi_i' \phi_j' dz \quad I_{1Bij} = \int_0^h \frac{1}{\rho} \phi_i \phi_j dz \quad I_2 =$$

$$I_{2ij} = \int_0^h \frac{1}{\lambda} \phi_i \phi_j dz$$

$$\frac{\partial I_1}{\partial c_i} = \frac{\partial I_{1A}}{\partial c_i} + \frac{\pi^2 m e}{a^2} \frac{\partial I_{1B}}{\partial c_i}$$

$$I_{1A} = \sum_j \sum_k c_j c_k I_{1Ajk} \quad \text{so} \quad \frac{\partial I_{1A}}{\partial c_i} = 2 \sum_k c_k I_{1Aik}$$

and so forth for  $I_{1B}$  and  $I_2$

$$\frac{\partial I_{1B}}{\partial c_i} = 2 \sum_k c_k I_{1Bik} \quad \frac{\partial I_2}{\partial c_i} = 2 \sum_k c_k I_{2ik}$$

$$\begin{bmatrix} I_{1A11} & I_{1A12} & \dots \\ \vdots & & \end{bmatrix} \begin{bmatrix} c_1 \\ c_2 \\ c_3 \\ \vdots \end{bmatrix} + \frac{\pi^2 m e}{a^2} \begin{bmatrix} I_{1B11} & \dots \\ \vdots & \end{bmatrix} \begin{bmatrix} c_1 \\ \vdots \end{bmatrix} = \omega^2 \begin{bmatrix} I_{211} & \dots \\ \vdots & \end{bmatrix}$$

$$\left( \underline{\underline{I}}_{1A} + \frac{\pi^2 m e}{a^2} \underline{\underline{I}}_{1B} \right) \underline{\underline{c}} = \omega^2 \underline{\underline{I}}_2 \underline{\underline{c}}$$



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$$I_{IAij} = \frac{(i-1/2)(j-1/2)\pi^2}{h^2} \int_0^h \frac{1}{\rho} \sin\left[\frac{(i-1/2)\pi z}{h}\right] \sin\left[\frac{(j-1/2)\pi z}{h}\right] dz$$

$$I_{IBij} = \int_0^h \frac{1}{\rho} \cos\left[\frac{(i-1/2)\pi z}{h}\right] \cos\left[\frac{(j-1/2)\pi z}{h}\right] dz$$

$$I_{2ij} = \int_0^h \frac{1}{\lambda} \cos\left[\frac{(i-1/2)\pi z}{h}\right] \cos\left[\frac{(j-1/2)\pi z}{h}\right] dz$$

$$\underline{\underline{I}}_2^{-1} \left( \underline{\underline{I}}_{IA} + \frac{\pi_{me}^2}{a^2} \underline{\underline{I}}_{IB} \right) \underline{\underline{C}} = \omega^2 \underline{\underline{C}}$$

$$\left[ \left( \underline{\underline{I}}_2^{-1} \underline{\underline{I}}_{IA} \right) + \frac{\pi_{me}^2}{a^2} \left( \underline{\underline{I}}_2^{-1} \underline{\underline{I}}_{IB} \right) \right] \underline{\underline{C}} = \omega^2 \underline{\underline{C}}$$

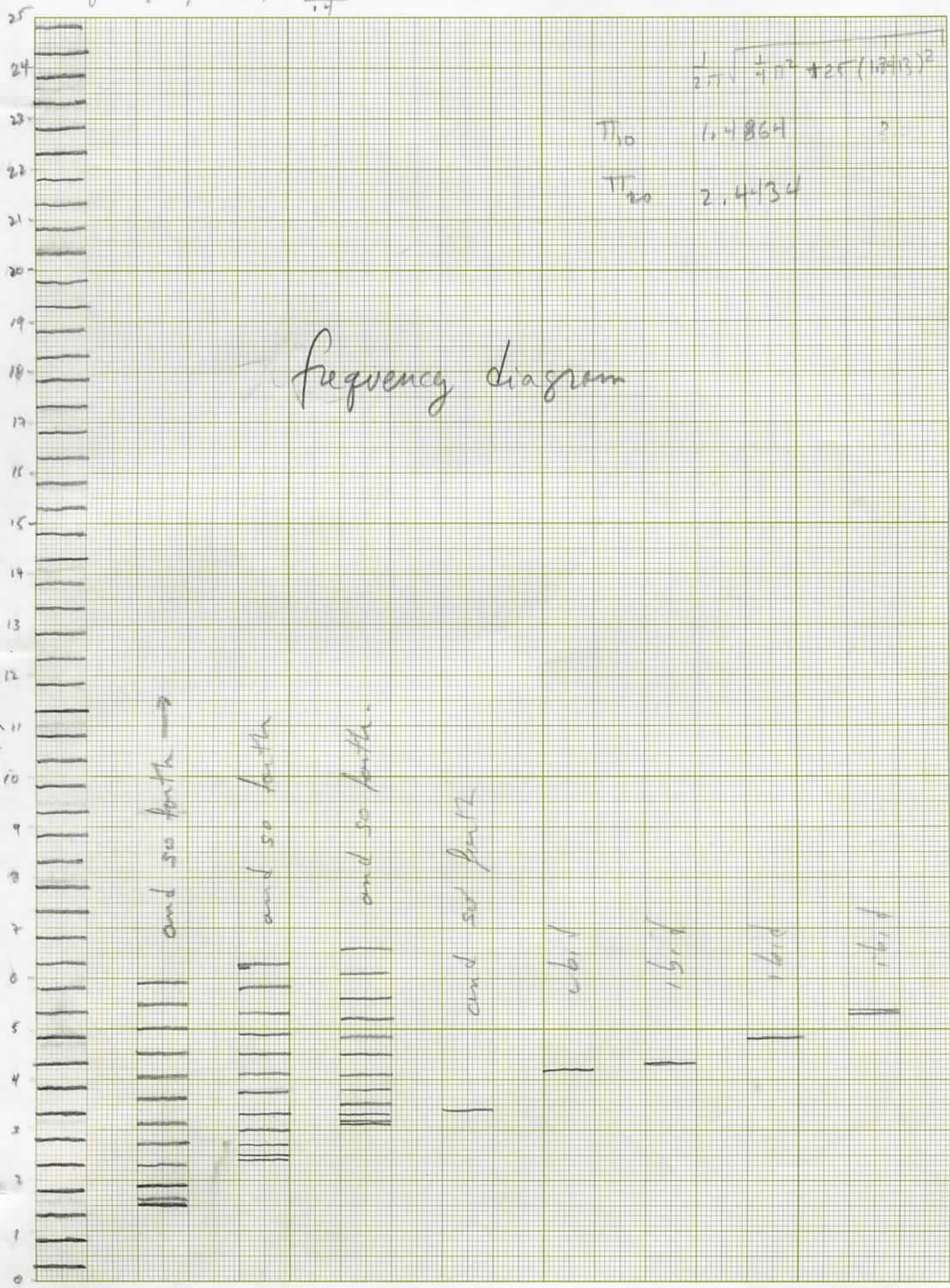


frequency for  $\omega = 1.0$   $\lambda=1, h=1, a=5$   $f = \frac{1}{2\pi} \sqrt{(n+\frac{1}{2})^2 \pi^2 + 25 \pi^2 m^2}$

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$f, \text{ Hz}$



frequency diagram

$$\frac{1}{2\pi} \sqrt{\frac{1}{4} \pi^2 + 25 (1.2113)^2}$$

$$\pi_{10} \quad 1.4864$$

$$\pi_{20} \quad 2.4134$$

$\pi_{00}$

$\pi_{10}$

$\pi_{20}$

$\pi_{01}$

$\pi_{30}$

$\pi_{11}$

$\pi_{40}$

$\pi_{50}$

$\pi_{21}$