Part 1 - Data Processing and Quality Control.

1. General
   a) Cruise Overview
      1) This cruise is a transit from South American to South Africa. After departing Punta Arenas, Chile, the track passes very close to the Falklands Islands, then south to the ice edge near 25°W, north to 33° N 14°W, then direct to Capetown, South Africa. Our data begin on 18 May and continue until 15 July, terminating near the edge of the South African 200 Mile Exclusive Economic Zone (EEZ).
      2) We have applied the revised algorithm for correcting for the time lag between water passing the remote temperature probe and arriving at our equilibrator. We move the pCO₂ data one scan earlier.

   b) Data Overview

   The pCO₂ data are excellent, and except for some questionable measurements associated with fluctuations in the flow of the water, little editing was required.

   The temperature probe in the pCO₂ system, as well as the Thermosalinograph (TSG) temperature probe, appeared to work flawlessly.
The salinity seems acceptable, but is UNCALIBRATED. Comparisons with Autosal measurements on previous cruises have shown an offset of as much as 0.3 units on the Practical Salinity Scale, so the accuracy of the salinities cannot be assured. Our experience aboard L.M. Gould, which has a similar system, shows that the salinity calibration will shift as the cell becomes contaminated in the first few days after cleaning, and then remain relatively steady for the remainder of the cruise.

The atmospheric $pCO_2$ observations were not well behaved. There is extensive spiking from what is probably stack gas contamination, and most of the observations were rejected.

c. Problems with the data.

1) Because of the heavy contamination of the air observations, we use the Globalview CO2 zonal average for the appropriate time and band to calculate the $pCO_2$ of air for use in calculating sea-air $pCO_2$ difference.

3) The data from Julian Day 194 is missing. It appears that no RVDAS data was recorded, or that file was corrupted. There is a raw $pCO_2$ data file for that date, but no JGOF format file.

2. Standards:

<table>
<thead>
<tr>
<th>Cylinder</th>
<th>Concentration (ppm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Nitrogen (UHP)</td>
<td>0.0</td>
</tr>
<tr>
<td>CA02231</td>
<td>236.29</td>
</tr>
<tr>
<td>CC51988</td>
<td>450.05</td>
</tr>
<tr>
<td>CC58080</td>
<td>151.67</td>
</tr>
<tr>
<td>CC15551</td>
<td>362.8</td>
</tr>
</tbody>
</table>

A 4th order calibration curve is used with 5 standards, including the Nitrogen, as described in Section 2.

Standards flow for about 120 seconds before an observation is made.

3. Details of $pCO_2$ data.

a) With the benefit of 10 plus years of observations, editing, and analysis, we have rejected the running mean as a criteria for rejecting “outliers.” These systems just do not work. It is impossible to account for the rapid changes occurring naturally in open ocean systems, with eddies, meandering of currents, local weather, and mesoscale weather and still retain valid observations. Essentially the file is hand edited.

b) There were 23,172 individual seawater $pCO_2$ observations. We rejected 418, retaining all 22,754 observations.

4. Details of temperature data.
a) The temperature of water in the equilibrator is monitored continuously using a Guildline platinum resistance thermometer (readable to 0.05 °C and regularly calibrated against a mercury thermometer traceable to N.I.S.T.) and recorded on the data-logging computer. The calibration curve is integrated into the LabVIEW program that operates the system and acquires the data. The pCO₂ temperature is then a calibrated value. We make an effort to check this calibration during cruises against a mercury thermometer.

b) The TSG temperature and the pCO₂ chamber gave a relationship as follows:

\[
\text{Sea Surface Temperature} = 1.0028 \times \text{pCO₂ Temperature} - 0.2481
\]

c) The documentation as received does not contain the serial numbers or calibration history of the TSG instrument.
5. Details of Salinity data.

   a) The salinity data are very reasonable during this cruise. Since there were no calibration samples taken, the absolute accuracy is undefined, however the structure of the data looks fine.

   b) The documentation as received does not contain the serial numbers or calibration history of the TSG instrument.

   c) The salinity data is UNCALIBRATED. Previous cruises where Autosal comparisons were available indicated as much as 0.3 units offset on the Practical Salinity Scale. The calibration seems to shift fairly rapidly, and by the end of 3-4 days, has probably settled into its new value. Therefore, the relative values, that is the excursions, are real and the base calibration is probably stable after that point.

6. Details of the air data

   As with the surface pCO₂ observations, with the benefit of an additional 10 years of observations, we have had to generally reject air observations from this ship. It is not possible to locate the observations contaminated by the ships exhaust systems, primarily from the main engines. Even with the benefit of accurate wind data, and trying to use a nearly head-on relative wind, we still get severe spikes in the air data. (added 03 Mar 2015).

   a) Generally speaking, these data were not unusual. There many positive spikes of the type normally associated with contamination from the ship's engine exhausts. It is difficult to filter these out, and we use a 3-pass mean and standard deviation type process. After each pass calculating the average of 9 observations, the data outside one standard deviation are rejected.

   b) Comparing these running average values to the Globalview equivalent is not meaningful as it is impossible to separate contaminated samples from uncontaminated ones.
Part 2 Description of Instrumentation

a) The LDEO Underway System for Surface Water pCO₂ Measurements:

The underway pCO₂ measurement system for surface waters consists of a) a water-air equilibrator, b) an analyzer system based on a non-dispersive infra-red CO₂ gas analyzer, c) sample pumps, d) 5 calibration standards and e) a data logging system. The measurement system is schematically shown in Fig. 1, and is similar with the one described in Bates et al. (1998). Each of these units and the data reduction procedures used will be described below.

Figure 2: Diagram of the underway pCO₂ system used for surface water pCO₂ measurements during NBP04-03 which is essentially identical to the Gould System.
b) **Water-air Equilibrator:**

The equilibrator has a total volume of about 30 liters and is equipped with a standpipe that is isolated from the headspace and automatically maintains a constant water level at about half the height of the equilibrator leaving about 15 liters of headspace (Figure 2). Seawater from the ship’s uncontaminated water line is continuously pumped into the equilibrator at a rate of about 10 liters/min, giving a mean residence time of water in the equilibrator of about 1.5 minutes. The headspace above the water serves as an equilibration chamber. A carrier gas (commonly marine air) is continuously circulated to and from the headspace in a closed loop by a diaphragm pump, and exchanges CO₂ with the continuous flow of seawater sprayed into the chamber through a spiral cone spray nozzle. Because of large gas-water contact areas created by fine water droplets as well as gas bubbles in the pool of water, CO₂ equilibration between the carrier gas and seawater is achieved rapidly with an e-folding time of 2 to 3 minutes. Under normal sampling conditions, about 50 ml/min of this sea water equilibrated air is directed into the infra-red gas analyzer. The air drawn for analysis is replaced by a controlled leak into the equilibrator through the water manometer. At this rate, the residence time of the carrier gas in the equilibration chamber is about 300 minutes, that is about 100 times as long as the equilibration time. Therefore, the carrier gas in the headspace should always be in equilibrium with the seawater. The over all response time of the equilibrator system has been estimated to be of an order of several minutes. The large volume of water in the equilibrator was chosen to provide a large thermal inertia in the equilibrator, so that the effects of room temperature changes on the equilibration temperature may be minimized. The temperature of water in the equilibrator is monitored continuously using a Guildline platinum resistance thermometer (readable to 0.05 °C and regularly calibrated against a mercury thermometer traceable to N.I.S.T.) and recorded on the data-logging computer.

The temperature and salinity of seawater at the *in situ* conditions were measured using a SeaBird Model SBE-21 thermosalinograph aboard the N. B. Palmer and a SIO/ODF thermosalinograph unit based on Neil Brown sensors aboard the R. Revelle. The precision of the reported temperature data has been estimated to be about 0.005 °C.

c) **Infra-red CO₂ Gas Analyzer:**

The equilibrated gas was passed through a water trap (to collect condensate,) and, and a reverse flow naphion dryer (PermaPure flushed with pure nitrogen gas) to remove water vapor (to a level of –20°C dewpoint), and was introduced into the IR sample cell at a rate of about 50 ml/min for CO₂ determinations. A LI-COR infra-red gas analyzer
(Model 6251, Lincoln, NB) was used. After a 2-minute purging period, the gas flow was stopped and readings were recorded on the computer. Although the CO2 analyzer has an electronic circuit to linearize the CO2 response, it exhibited a few inflexions that deviated from linearity by a few ppm. Therefore, the pCO2 system has been designed to use the raw voltage output of the CO2 analyzer to establish our own calibration curves using five standard gas mixtures (one pure nitrogen and four CO2-air mixtures). The CO2 concentrations in the gas mixtures were calibrated using the SIO standards determined by C. D. Keeling’s group using the manometric method. The concentrations of CO2 in the standard gas mixtures were summarized above.

During normal operations approximately every 75 minutes each of the standard gas mixtures was passed through the analyzer for 120 seconds at a rate of about 60 ml/min. This flow rate and time was redundantly sufficient to completely purge the IR analyzer cell with the new gas. The flow was stopped for 10 seconds to allow the pressure in the cell to equilibrate to atmospheric pressure and the average of 20 separate millivolt readings from the analyzer was recorded. Following the five standard gases, samples of seawater-equilibrated air and ambient marine air were pumped through the analyzer for 120 seconds (2 minutes) each at rates of about 50 ml/min and 60 ml/min respectively to purge the previous sample in the IR cell. The flow was stopped for 10 seconds and the average of 20 separate millivolt readings from the analyzer was recorded. This procedure was intended to eliminate errors due to fluctuations of the dynamic pressure within the IR cell by irregular gas flow rates. The relatively slow flow rates used for seawater-equilibrated air samples were required for the removal of water vapor using the PermaPure membrane dryer. We analyze 30 seawater-equilibrated air samples and 5 ambient marine air samples between two sets of calibration runs using the five standard gases.

d) Data Logging System:

The following values were recorded on a laptop computer. The sample locations were derived from the ships Global Positioning System (GPS). The CO2 readings for seawater equilibrated air samples were recorded approximately every 3 minutes, and those for the standard gas mixtures approximately every 90 minutes.

Time/Date stamp (GMT),
CO2 analyzer voltage output (to 0.1 mv)
Analyzer cell temperature (to 0.1 C)
Barometric pressure (pCO2 system barometer) (to 0.1 mbar)
CO2 concentration (to 0.1 ppm, preliminary value based on the last response curve)
Equilibrator temperature (to 0.01 °C)
pCO2 (uatm, preliminary value based on the last response curve)
Gas flow rate (to 0.1 cc/min)
Selector valve position (integer)
Sample ID (standard gas cylinder numbers, seawater CO2, atmospheric CO2)
The ships RVDAS system adds several other data elements from various sensors and equipment including: Latitude, Longitude, Thermosalinograph temperature, thermosalinograph salinity, fluorometer voltage, wind speed, wind direction, barometric pressure (at ships instrument mast), water flow in the uncontaminated seawater line.

e) Data Reduction Procedures:

The concentration of CO2 in the sample was computed in the following manner based on the millivolt reading and time of the reading. The millivolt reading taken for each of the five standard gases at the time of sample measurement was computed by linearly interpolating as a function of time using the readings taken before and after the respective standard gases were analyzed. This yields an interpolated millivolt reading for each of the five standard gases at the time when the sample was analyzed. These five values were fit to a fourth-order polynomial equation (with five constants to be determined). This serves as the response curve. The CO2 concentration in the sample was computed using the response curve that was established at the time of each sample analysis. This method has been demonstrated to yield more reliable CO2 values compared with those computed, for example, using a least-squares fit of a quadratic or cubic functions to the five calibration points. The method described above yields atmospheric CO2 values that are consistent (within 1.5 ppm) with those reported for the South Pole and the Cape Grim by the Climate Monitoring and Diagnostics Laboratory/NOAA in Boulder, CO.

The partial pressure of CO2 in seawater, (pCO2)sw, at the temperature of equilibration, Teq, in the unit of microatmospheres (µatm) was computed using the expression:

\[(pCO2)sw @ Teq = (VCO2)eq \times (Peq – Pw)\]  \[\ldots \]  \[\ldots \]  \[\ldots \] \[1\]

\((VCO2)eq\) = the mole fraction concentration (ppm) of CO2 in the dried equilibrated carrier gas;

\(Peq\) = the barometric pressure (that is equal to the total pressure of equilibration) in atmospheres; and

\(Pw\) = the equilibrium water vapor pressure at Teq (°C) and salinity.

The water vapor pressure was computed using the following formulation;

\[Pw \text{ (atm)} = (1/760)x(1 – 5.368x10^{-4}x Sal)\]
\[\times \text{ EXP}\{[0.0039476 – (1/TK)]/1.8752x10^{-4}\}, \ldots \] \[\ldots \] \[\ldots \] \[2\]

where \(Sal\) is salinity on the Practical Salinity Scale and measured using the ship’s thermosalinograph, and \(TK\) is the temperature of equilibration in °K.

The \((pCO2)sw\) at the \textit{in situ} temperature, \(T \textit{ in situ}\), was computed using a constant value of 0.0423 % per °C for the effect of temperature (Takahashi et al., 1993):
\[(p\text{CO}_2)_{\text{sw}} @ \text{In situ} = (p\text{CO}_2)_{\text{sw}} @ \text{Teq} \times \exp[0.0423 \times (\text{T}_{\text{in-situ}} - \text{Teq})].\]

The value for \text{In situ} is taken to be the seawater temperature measured by the ship’s thermosalinograph at the time of pCO\textsubscript{2} measurements. Teq is generally warmer than \text{In-situ} by 0.5 ~ 0.8 °C. Hence the temperature correction is normally less than 3% of pCO\textsubscript{2} values.

The overall precision of the reported (pCO\textsubscript{2})\textsubscript{sw} values has been estimated to be about ±1.5 uatm.

**f) Atmospheric Measurements:**

The air measurement system is also shown schematically in Fig. 1. Uncontaminated marine air samples were collected about 10 m above the sea surface using a 1/4” i.d. thin-walled aluminum tubing protected by an exterior plastic casing and an internal plastic film lining (Synflex, Calco Inc., PA). The air intake was located at the middle of the foremast about 10 m above the sea surface. A KNF Neuberger air pump located near the IR analyzer was used to pump air through the tubing and into the IR analyzer. Even when air samples were not analyzed, air was continually flowing through the sampling line to continuously purge the long Synflex tubing with fresh marine air. For analysis, the air sample was passed through a 0.5 micron filter to remove aerosols and a drying column to remove water vapor (the same PermaPure column as used for the seawater-equilibrated air) and introduced into the IR cell for CO\textsubscript{2} analysis at a rate of about 60 ml/min. For each sample the cell was purged for 120 seconds, the flow was stopped for 10 seconds and the average of 20 IR millivolt output readings was recorded on the computer.

**g) Atmospheric Data Processing:**

The partial pressure of CO\textsubscript{2} in the air, \((p\text{CO}_2)_{\text{air}}\), was computed in the unit of microatmospheres (µatm) in the same way as that for seawater using Eq. [3] below:

\[(p\text{CO}_2)_{\text{air}} = (V\text{CO}_2)_{\text{air}} \times (P_b - P_w), \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots [3]\]

\((V\text{CO}_2)_{\text{air}}\) = the mole fraction concentration (ppm) of CO\textsubscript{2} in the dried air sample;

\(P_b\) = the barometric pressure at sea surface in atmospheres; and

\(P_w\) = the equilibrium water vapor pressure at \text{in situ} (°C) and salinity given by Eq. [2].

The precision of the atmospheric pCO\textsubscript{2} values have been estimated to be about ± 1 µatm.
Part 3 - References


PART 4 - Graphics

List of Figures:

A Map showing the location of each seawater pCO$_2$ value with the data point assigned a color based on an indicated color palette.

Ten 3-panel time series of various parameters, five each for the southbound and northbound legs.

A time series showing salinity data with editing.

A time series showing the air data with editing.

A pair of plots comparing the VCO$_2$ of dry air as observed by the LDEO system (after filtering).
Part 5 - Program Listings

These listings provide detailed documentation of processes applied to the data, including the calculation of a response curve, editing, and certain quality control operations.